

# Performance measurement of a

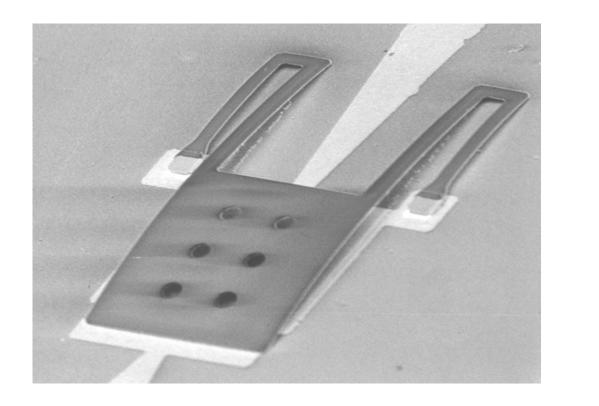
## commerical PbSe photoconductor

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#### Motivation

We are in development of a radiant energy imager using MEMS cantilevers in a null-position clocking design. Work is based on US Patent No 7977635 (2011) by Oliver Edwards.



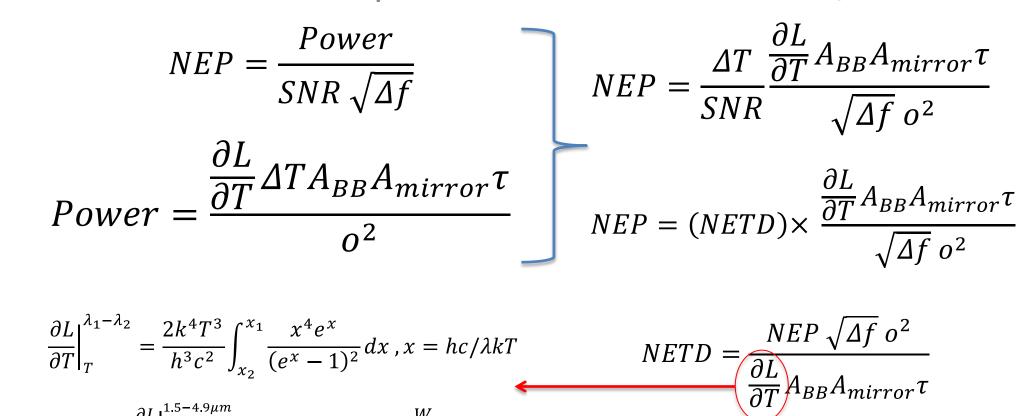
#### NEP and NETD

Noise Equivalent Power (NEP) - The amount of radiant power incident that results in a signal to noise ratio (SNR) of 1.  $NEP = \frac{Incident\ Power}{}$ 

- Used to characterize a single detector
- Noise Equivalent Temperature Difference (NETD) The difference between target temperature and background that yeilds SNR=1.
- Used to characterize an array of detectors or an entire IR system •  $NETD = \frac{\Delta T}{\Omega}$ SNR Smaller NEP and NETD mean better resolution

### Calculation of NETD

Detector Manual specifies NEP= 1.5 x 10<sup>-10</sup> W/VHz



Current calculated performance measures are:

- 3.6 mK NETD with F/1 optics and a 30 Hz bandwidth
- *Time* responsivity of 80 nsec per 1°C or 21 nsec per nWatt incident energy, requiring greater than 12.5 GHz clock pulse for 1mK LSB.
- 1 KHz frame rate

These performance measures need experimental evidence. Demonstration of performance measurements of commercial detectors will validate the experimental technique of measuring the above theoretical claims.

Both depend upon the electronic bandwidth  $\Delta f$ . Noise power increases proportional to  $\Delta f$ , noise voltage is proportional to  $V\Delta f$ . Therefore is is useful to define NEP as power per root bandwidth (W/VHz)



Δf=1.25 kHz (<sup>1</sup>/<sub>2</sub> the sampling frequency of the trace on the oscilloscope

 $NETD = \frac{1.5 \times 10^{-10} \times \sqrt{1250} \times 30^2}{3.96 \times 10^{-6} \times 0.78 \times 17.3 \times 0.9}$ 

Noise (mV)

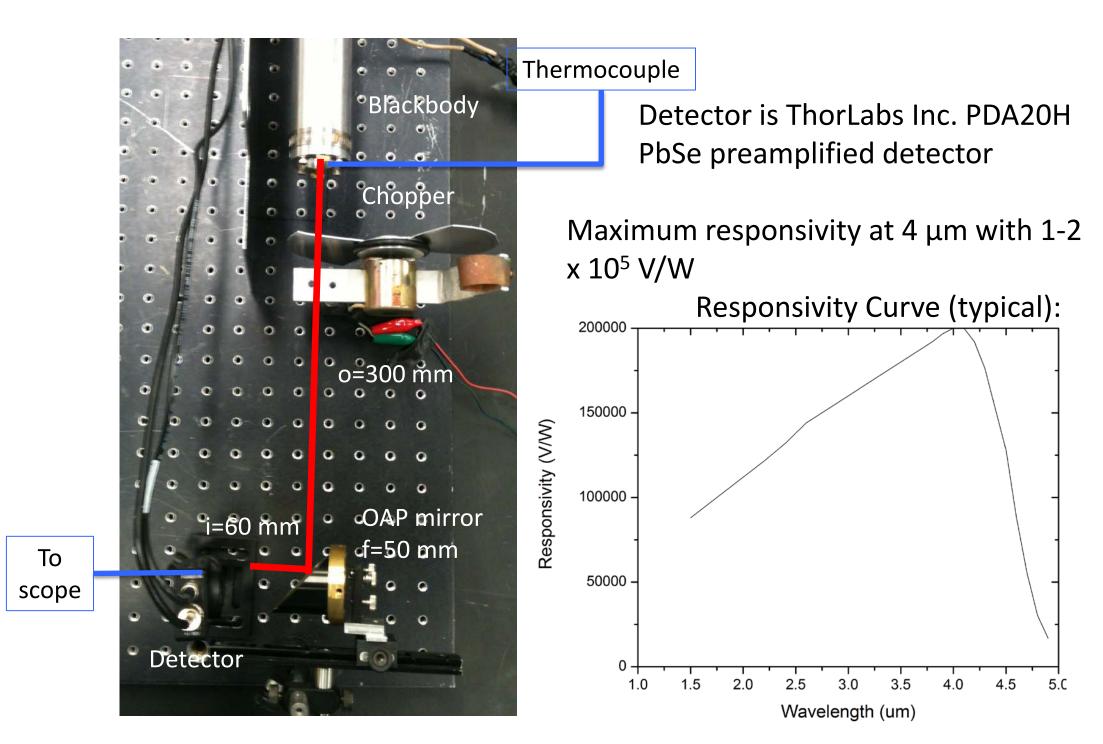
1.87

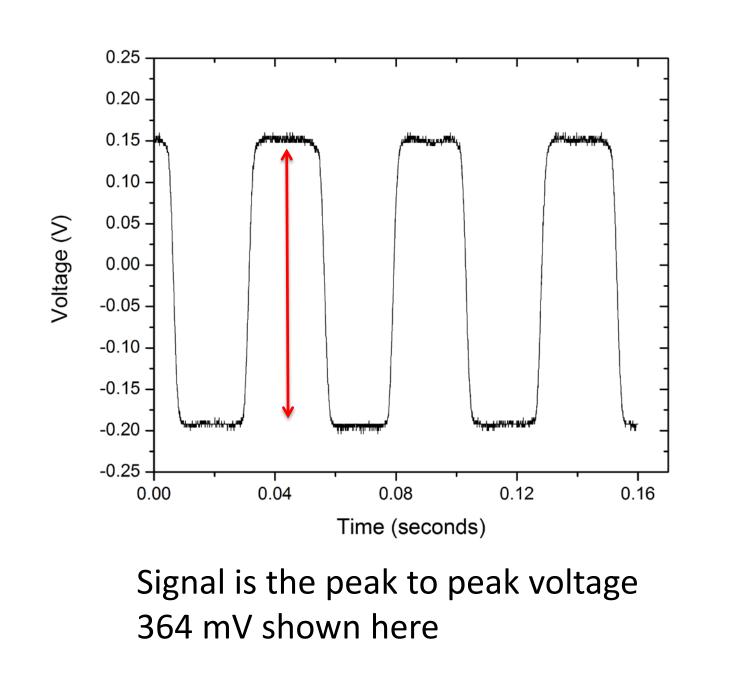
1.83

•  $\tau = 90\%$  (transmission of the atmosphere)

## **Experiment Design and Results**

The experiment design is based on ASTM E1543 for measuring NETD. A 1 cm diameter aperture blackbody with 20°C<ΔT<150°C is modulated by a chopper at 20 Hz. An OAP mirror focuses radiation onto the PbSe detector active area (2x2 mm)





**ΔT** (°C)

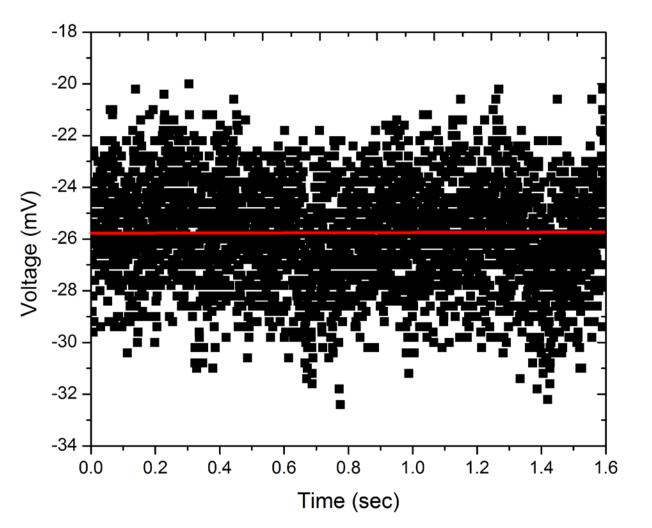
41.1

55.7

Signal (mV)

364

656



SNR

195

358

 $\neq$  99 mK

NETD (mK)

210

155

#### Radiance

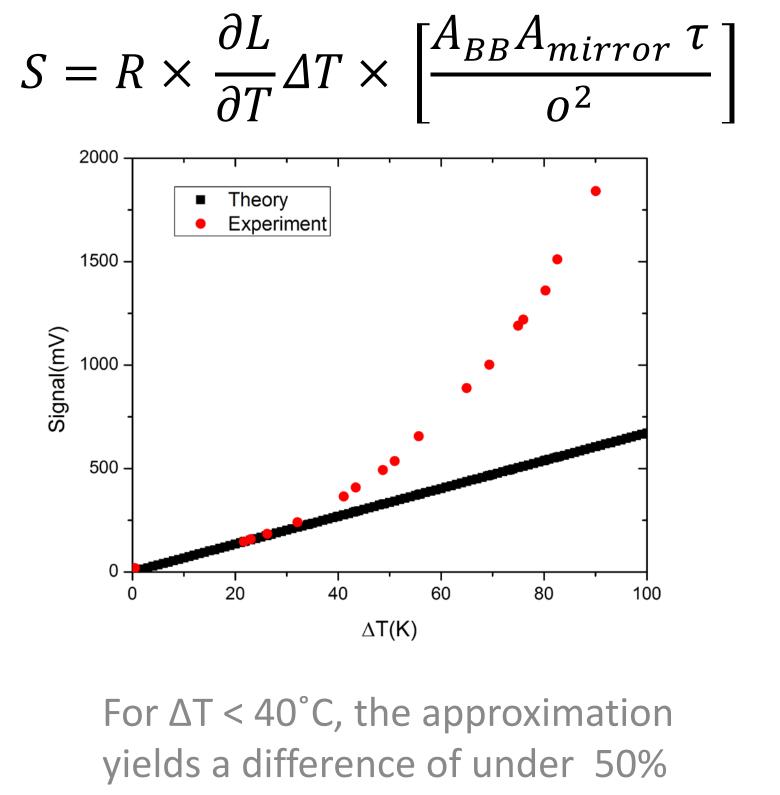
Radiance is the power emitted by a blackbody per unit area per unit solid angle and is described by Planck's Law

$$L = +\frac{2k^4T^4}{h^3c^2} \int_{x^2}^{x^1} \frac{x^3}{e^x - 1} dx \approx \frac{\partial L}{\partial T} \Delta T$$

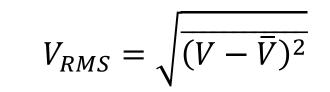
The approximation shown above, also used in the NETD derivation, is valid for small  $\Delta T$ . This can be verified by calculating the signal based upon the detector responsivity, and comparing to experimental data

Calculated Signal:

as



Noise is found by blocking the blackbody and measuring the background Noise voltage is the RMS variance:

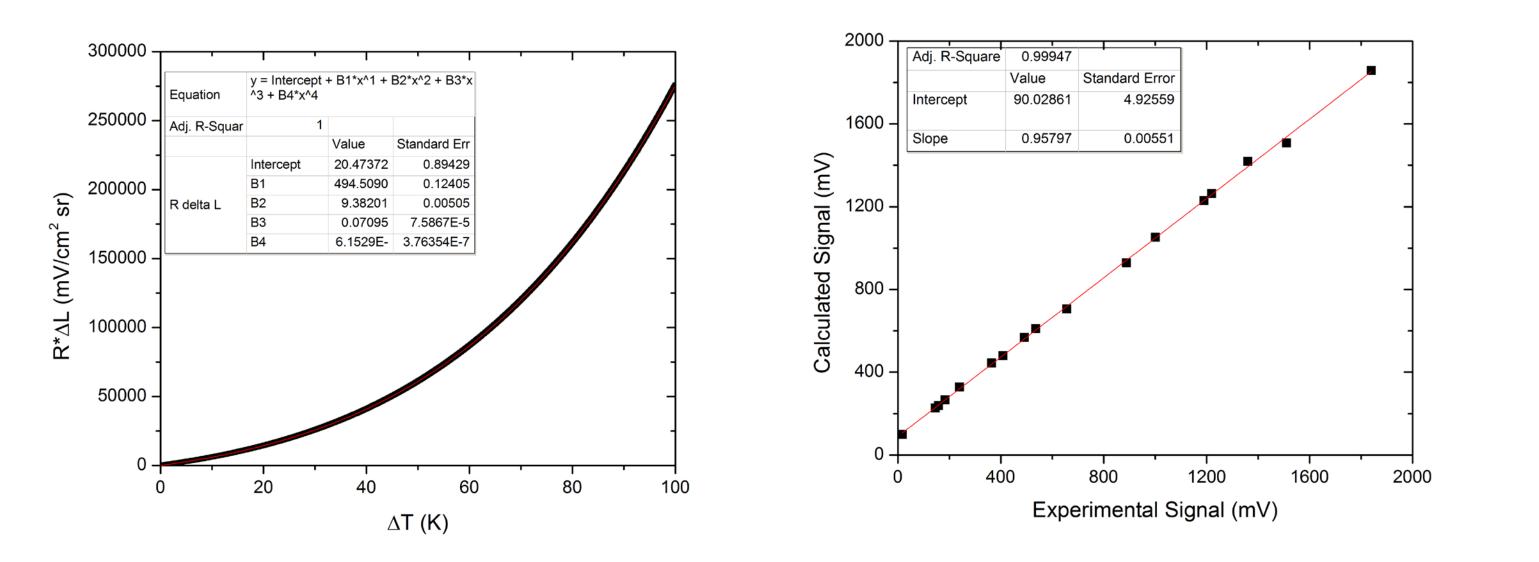


## **Corrected Radiance**

The more accurate way to describe the signal mathematically is to integrate the product of the responsivity curve by the radiance curve over the wavelength interval of the detector:

 $\int \left( R_{\lambda} L_{\lambda}(T_{BB}) - R_{\lambda} L_{\lambda}(T_{ref}) \right) d\lambda$ 

The calculated signal can be approximated as a 4<sup>th</sup> order polynomial and matches with experimental data:



#### Future Work

- Integrate a faster chopper (f > 600 Hz) and a lock-in amplifier to reduce the noise level and the bandwidth to measure smaller NETD
- Repeat experiment with IR camera systems
- Adapt the experiment to measure clocking duty cycles rather than



